

# **Anholonomic Configuration Spaces and Metric Tensors in Finite Elastoplasticity**

by John D. Clayton, David L. McDowell, and Douglas J. Bammann

ARL-RP-118 February 2006

A reprint from the *International Journal of Non-Linear Mechanics*, vol. 39, pp. 1039–1049, 2004.

# **NOTICES**

# **Disclaimers**

The findings in this report are not to be construed as an official Department of the Army position unless so designated by other authorized documents.

Citation of manufacturer's or trade names does not constitute an official endorsement or approval of the use thereof.

Destroy this report when it is no longer needed. Do not return it to the originator.

# **Army Research Laboratory**

Aberdeen Proving Ground, MD 21005-5066

ARL-RP-118 February 2006

# **Anholonomic Configuration Spaces and Metric Tensors in Finite Elastoplasticity**

John D. Clayton Weapons and Materials Research Directorate, ARL

> David L. McDowell Georgia Institute of Technology

Douglas J. Bammann Sandia National Laboratories

A reprint from the *International Journal of Non-Linear Mechanics*, vol. 39, pp. 1039–1049, 2004.

Approved for public release; distribution is unlimited.

# REPORT DOCUMENTATION PAGE

## Form Approved OMB No. 0704-0188

Public reporting burden for this collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing the burden, to Department of Defense, Washington Headquarters Services, Directorate for Information Operations and Reports (0704-0188), 1215 Jefferson Davis Highway, Suite 1204, Arlington, VA 22202-4302. Respondents should be aware that notwithstanding any other provision of law, no person shall be subject to any penalty for failing to comply with a collection of information if it does not display a currently valid OMB control number.

PLEASE DO NOT RETURN YOUR FORM TO THE ABOVE ADDRESS.

1. REPORT DATE (DD-MM-YYYY)	2. REPORT TYPE	3. DATES COVERED (From - To)	
February 2006	Reprint	1 January 2003–1 January 2006	
4. TITLE AND SUBTITLE		5a. CONTRACT NUMBER	
Anholonomic Configuration Space			
		5b. GRANT NUMBER	
		5c. PROGRAM ELEMENT NUMBER	
6. AUTHOR(S)	5d. PROJECT NUMBER		
` '			
John D. Clayton, David L. McDo	well, and Douglas J. Bammann	1L1622618AH80	
		5e. TASK NUMBER	
		5f. WORK UNIT NUMBER	
7. PERFORMING ORGANIZATION NAME	8. PERFORMING ORGANIZATION		
U.S. Army Research Laboratory		REPORT NUMBER	
ATTN: AMSRD-ARL-WM-TD	ARL-RP-118		
Aberdeen Proving Ground, MD 2			
9. SPONSORING/MONITORING AGENCY NAME(S) AND ADDRESS(ES)		10. SPONSOR/MONITOR'S ACRONYM(S)	
		11. SPONSOR/MONITOR'S REPORT	
		NUMBER(S)	

#### 12. DISTRIBUTION/AVAILABILITY STATEMENT

Approved for public release; distribution is unlimited.

#### 13. SUPPLEMENTARY NOTES

A reprint from the International Journal of Non-Linear Mechanics, vol. 39, pp. 1039–1049, 2004.

George W. Woodruff School of Mechanical Engineering, Georgia Institute of Technology, Atlanta, GA 30332-0405.

Department of Science-based Materials Modeling, Sandia National Laboratories, Livermore, CA 94551.

#### 14. ABSTRACT

Deformation mappings are considered that correspond to the motions of lattice defects, elastic stretch and rotation of the lattice, and initial defect distributions. Intermediate (i.e., relaxed) configuration spaces associated with these deformation maps are identified and then classified from the differential-geometric point of view. A fundamental issue is the proper selection of coordinate systems and metric tensors in these configurations when such configurations are classified as anholonomic. The particular choice of a global, external Cartesian coordinate system and corresponding covariant identity tensor as a metric on an intermediate configuration space is shown to be a constitutive assumption often made regardless of the existence of geometrically necessary crystal defects associated with the anholonomicity (i.e., the non-Euclidean nature) of the space. Since the metric tensor on the anholonomic configuration emerges necessarily in the definitions of scalar products, certain transpose maps, tensorial symmetry operations, and Jacobian invariants, its selection should not be trivialized. Several alternative (i.e., non-Euclidean) representations proposed in the literature for the metric tensor on anholonomic spaces are critically examined.

#### 15. SUBJECT TERMS

elastoplasticity, incompatibility, configurations

16. SECURITY CLASSIFICATION OF:		17. LIMITATION OF ABSTRACT	18. NUMBER OF PAGES	19a. NAME OF RESPONSIBLE PERSON John D. Clayton	
a. REPORT	b. ABSTRACT	c. THIS PAGE	1 111	1.0	19b. TELEPHONE NUMBER (Include area code)
UNCLASSIFIED	UNCLASSIFIED	UNCLASSIFIED	UL	18	(410) 306-0975



## Available online at www.sciencedirect.com



International Journal of Non-Linear Mechanics 39 (2004) 1039-1049



# Anholonomic configuration spaces and metric tensors in finite elastoplasticity

J.D. Clayton<sup>a,1</sup>, D.J. Bammann<sup>b</sup>, D.L. McDowell<sup>a,\*</sup>

<sup>a</sup> George W. Woodruff School of Mechanical Engineering, Georgia Institute of Technology, Atlanta, GA 30332-0405, USA
<sup>b</sup> Department of Science-based Materials Modeling, Sandia National Laboratories, Livermore, CA 94551, USA

Accepted 2 June 2003

#### Abstract

Deformation mappings are considered that correspond to the motions of lattice defects, elastic stretch and rotation of the lattice, and initial defect distributions. Intermediate (i.e., relaxed) configuration spaces associated with these deformation maps are identified and then classified from the differential-geometric point of view. A fundamental issue is the proper selection of coordinate systems and metric tensors in these configurations when such configurations are classified as anholonomic. The particular choice of a global, external Cartesian coordinate system and corresponding covariant identity tensor as a metric on an intermediate configuration space is shown to be a constitutive assumption often made regardless of the existence of geometrically necessary crystal defects associated with the anholonomicity (i.e., the non-Euclidean nature) of the space. Since the metric tensor on the anholonomic configuration emerges necessarily in the definitions of scalar products, certain transpose maps, tensorial symmetry operations, and Jacobian invariants, its selection should not be trivialized. Several alternative (i.e., non-Euclidean) representations proposed in the literature for the metric tensor on anholonomic spaces are critically examined. © 2003 Elsevier Ltd. All rights reserved.

Keywords: Elastoplasticity; Incompatibility; Configurations

#### 1. Introduction

The notion of a relaxed "intermediate" or "natural" configuration in finite deformation anelasticity or elastoplasticity, wherein each local crystal volume element exhibits a stress-free state, was forwarded by many researchers in the mid-20th century [1–8]. Such a relaxed configuration may correspond to the intermediate configuration arising from the usual

multiplicative decomposition of the deformation gradient [9,10], with the relaxed state associated with the local unloading of each volume element from its stressed state in the *current* (i.e., deformed or Eulerian) configuration. Alternatively, the relaxed configuration may correspond to local unloading of each volume element from its *reference* (i.e., initial or Lagrangian) state; such a natural configuration will differ from the initial configuration when the body contains a distribution of internal residual stress fields associated with crystal defects, for example [11,7,12].

It is important to note that in most cases the stress-free configuration is only locally coherent (i.e., simply connected or *holonomic*), since each volume element that undergoes relaxation will deform during

<sup>\*</sup> Corresponding author. Tel.: +1-404-894-5128; fax: +1-404-894-3203.

E-mail address: david.mcdowell@me.gatech.edu (D.L. McDowell).

<sup>&</sup>lt;sup>1</sup> Current address: Impact Physics Branch, Army Research Laboratory, Aberdeen Proving Ground, MD 21005-5069, USA.

the unloading process in a fashion that is incompatible with the relaxation deformations of its neighboring elements. In other words, a crystalline body supporting a distribution of heterogeneous internal stress fields associated with defects must generally be cut into multiple pieces in order to simultaneously relieve the stress in every piece. The ensemble of pieces comprises, in differential-geometric terminology, an anholonomic space [13,14], or a space that does not admit a homeomorphism (i.e., an invertible, bi-continuous, one-to-one mapping) to coordinates of a three-dimensional Euclidean space, the latter being the geometric space occupied by the coherent crystalline body prior to local stress relaxation. It is also understood stresses are relaxed to zero only in an average sense in the so-called "stress-free" configuration. In other words, when traction is removed from the external surface of each local volume element, self-equilibrating forces may still be present internally, within each element. Total relaxation of all internal forces (e.g., atomic and sub-atomic level interactions) can only be achieved at observation scales more far more refined than those describable by continuum elastoplasticity theories.

A well-known fact from differential geometry is that for a manifold (i.e., configuration space) to admit a single global Cartesian coordinate frame whose basis vectors are tangent to curves on the manifold, the space must be Euclidean [13,15]. Necessarily associated with the Euclidean property of the space is vanishing of the Riemann-Christoffel curvature tensor constructed from partial derivatives of the metric tensor of the coordinate system, with the metric tensor corresponding to the covariant identity tensor (i.e., a covariant Kronecker's delta) when a single Cartesian frame is selected. On the other hand, when the space is non-Euclidean (e.g., anholonomic), prescription of the Cartesian metric tensor implying a single set of three orthonormal basis vectors spanning the global anholonomic space may be an inappropriate assumption when such basis vectors are identified as tangents to the material manifold in the intermediate configuration [16]. In recognition of this issue, alternative covariant deformation measures (e.g., elastic, plastic, or total strain tensors) have been implemented as metric tensors for the purpose of lowering indices on contravariant quantities referred to anholonomic spaces [17-20].

In this work we first review the criteria for labeling a space as either holonomic or anholonomic and show how such spaces arise in finite elastoplasticity. We next demonstrate reasons why a metric tensor on the anholonomic configuration must often be specified: to define the transpose operation for mixed-variant tensors, to conduct symmetry operations on nominally mixed-variant tensors, to define Jacobian invariants of deformation mappings, and to define scalar products of vectors and contravariant tensors referred to the anholonomic space. Finally, several alternative choices for the anholonomic configuration coordinate system and associated metric tensor are presented and then critically evaluated within the context of finite elastoplasticity.

# 2. Anholonomic configurations in finite elastoplasticity

Consider the following multiplicative decompositions for the total deformation gradient **F** [21]:

$$\mathbf{F} = \mathbf{F}^{\mathbf{e}} \mathbf{F}^{\mathbf{p}} = \mathcal{K} \mathcal{K}_{0}^{-1},$$

$$F_{A}^{a} = F_{\alpha}^{\mathbf{e}^{a}} F_{A}^{\mathbf{p}^{a}} = \mathcal{K}_{\alpha}^{a} \mathcal{K}_{0A}^{-1^{a}},$$
(1)

where the associated configurations and local tangent spaces are illustrated in Fig. 1, and where all indices

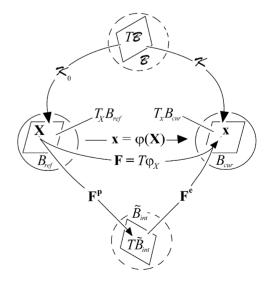


Fig. 1. Configurations and tangent maps.

 $a, A, \alpha, \alpha = 1, 2, 3$ . We label the reference configuration (i.e., the initial state) as  $B_{ref}$ , the current configuration (i.e., deformed state) as  $B_{\text{cur}}$ , the intermediate configuration of finite elastoplasticity (i.e., the relaxed state achieved via locally unloading from the current configuration) as  $\tilde{B}_{int}$ , and the *natural* configuration (i.e., the relaxed state achieved via local unloading from the reference configuration) as 3. Local unloading from the reference configuration is associated with relaxation of internal stress fields corresponding to dislocations and other defects present within the crystal(s) at the initial time, when the entire crystalline body is typically assumed to be free of external traction. Local unloading from the current configuration corresponds to simultaneous relaxation of internal stress fields due to dislocations and other defects present at the current time as well as any traction applied to the external surface of the crystalline body. As mentioned already, the particular relaxed configuration attained depends strongly upon the size of each local volume element, and the so-called "internal stress fields" that are relaxed here may be viewed as stresses arising from the traction applied externally to the surface of each local volume element. The elastic and plastic tangent maps of multiplicative elastoplasticity are written in Eq. (1) as  $\mathbf{F}^{e}$  and  $\mathbf{F}^{p}$ , respectively. The tangent map  $\mathcal{K}_{0}$  links the natural and reference configurations, while the tangent map  $\mathcal{K}$  links the natural and current configurations. We remark that while some authors have multiplicatively decomposed our  $\mathcal{K}$  into elastic and plastic parts [22,12], we find the decomposition (1) more convenient in the present setting, since in our approach the covariant leg of  $\mathbf{F}^p$  is referred to the Euclidean space  $B_{ref}$ . In precise terms, when defined in terms of stress relaxation, the (inverse of the) elastic tangent map Fe is characterized only up to an arbitrary rotation tensor [10]. Some aspect of the microstructure is needed to specify the elastic (or plastic) rotation, such as local lattice orientation in classical crystal plasticity theories, for example (cf. [12]).

We require in the present work for **F** to be *compatible* (i.e., integrable, holonomic, or a *true* deformation gradient):

$$\mathbf{F} = \frac{\partial \mathbf{x}}{\partial \mathbf{X}}, \quad F_A^a = \frac{\partial x^a}{\partial X^A}, \tag{2}$$

where  $\mathbf{x}$  and  $\mathbf{X}$  are current and reference coordinates, respectively, the former assumed to be smooth single-valued functions of the latter and time t. Following directly from (2), certain integrability conditions are automatically fulfilled:

$$F^{a}_{.A,B} = \frac{\partial^{2} x^{a}}{\partial X^{A} \partial X^{B}} = \frac{\partial^{2} x^{a}}{\partial X^{B} \partial X^{A}}$$
$$= F^{a}_{.B,A} \to F^{a}_{.A,B} - F^{a}_{.B,A} \equiv 2F^{a}_{.[A,B]} = 0, \qquad (3)$$

where, as shown, the subscripted comma denotes partial coordinate differentiation and the bracketed indices are anti-symmetrized.

In contrast to  $\mathbf{F}$ , the deformation maps  $\mathbf{F}^e$ ,  $\mathbf{F}^p$ ,  $\mathcal{K}$ , and  $\mathcal{K}_0$  generally *do not* fulfill conditions analogous to (2) and (3); i.e., these maps are generally not integrable. In fact, the lack of their integrability is often associated with the presence of crystal defects (cf. [4,5]). For example, consider the line integral of the differential vector element  $d\mathbf{\tilde{x}} \equiv \mathbf{F}^p d\mathbf{X}$  about a closed contour  $\tilde{c}$  in  $\tilde{B}_{int}$ :

$$\tilde{b}^{\alpha} \equiv \oint_{\tilde{c}} d\tilde{x}^{\alpha} = \oint_{C} F_{A}^{p^{\alpha}} dX^{A}$$

$$= -\int_{A} F_{[A,B]}^{p^{\alpha}} dX^{A} \wedge dX^{B}, \tag{4}$$

where we have assumed Cartesian coordinates  $X^A \in B_{\text{ref}}$  and invoked Stokes' theorem (cf. [13,23]) to convert from a line integral to a surface integral over the area A enclosed by the loop C (the image of  $\tilde{c}$  in  $B_{\text{ref}}$ ), and where the skew-symmetric rank 2 differential area element is denoted by  $\mathrm{d}X^A \wedge \mathrm{d}X^B$ . In Eq. (4),  $\tilde{\mathbf{b}}$  is typically called the *net Burgers vector* of all geometrically necessary dislocations piercing the area A at the current time. Equivalently, we may write for  $\tilde{\mathbf{b}}$ 

$$\tilde{b}^{\alpha} \equiv \oint_{\tilde{c}} d\tilde{x}^{\alpha} = \oint_{c} F_{.a}^{e-1^{\alpha}} dx^{a}$$

$$= -\int_{a} F_{.[a,b]}^{e-1^{\alpha}} dx^{a} \wedge dx^{b}$$
(5)

in terms of the inverse of the tangent map  $\mathbf{F}^e$  and the area element  $\mathrm{d} x^a \wedge \mathrm{d} x^b$  in the current configuration. We see from (5) that the anholonomicity of  $\tilde{B}_{\mathrm{int}}$  is directly related to defects present within the crystal at the *current time*, since configuration  $\tilde{B}_{\mathrm{int}}$  is defined in terms of local elastic unloading from  $B_{\mathrm{cur}}$ . It should

be noted that while Eq. (4) defines  $\tilde{\mathbf{b}}$  in terms of differentiation and line and area elements referred to the reference configuration,  $\tilde{\mathbf{b}}$  of (4) is equivalent to  $\tilde{\mathbf{b}}$  of (5) and is *not* indicative of internal stress fields due to dislocations present at the *initial time*. Instead, we must define a different net Burgers vector  $\ell$  quantifying the anholonomicity of configuration  $\mathcal{B}$  and representative of the defect densities present within the crystal at the initial time (since  $\mathcal{B}$  is defined in terms of local elastic unloading from the initial state  $B_{\text{ref}}$ ):

$$\ell^{a} \equiv \oint_{c} dx^{a} = \oint_{c} \mathcal{K}_{.a}^{-1^{a}} dx^{a}$$

$$= -\int_{a} \mathcal{K}_{.[a,b]}^{-1^{a}} dx^{a} \wedge dx^{b},$$

$$\ell^{a} \equiv \oint_{c} dx^{a} = \oint_{C} \mathcal{K}_{0.A}^{-1^{a}} dX^{A}$$

$$= -\int_{a} \mathcal{K}_{0.[A,B]}^{-1^{a}} dX^{A} \wedge dX^{B},$$
(6)

where  $\varepsilon$  is a closed circuit in the natural configuration  $\mathcal{B}$ . In the interest of brevity, subsequent equations will focus upon the multiplicative decomposition  $\mathbf{F} = \mathbf{F}^{\mathrm{e}} \mathbf{F}^{\mathrm{p}}$  and the associated anholonomic space  $\tilde{B}_{\mathrm{int}}$ ; however, our arguments will generally also apply to the decomposition  $\mathbf{F} = \mathcal{K} \mathcal{K}_0^{-1}$  and the corresponding anholonomic space  $\mathcal{B}$ .

Basis vectors locally tangent to the Euclidean spaces  $B_{\text{ref}}$  and  $B_{\text{cur}}$ , respectively, are written

$$\mathbf{G}_A \equiv \frac{\partial}{\partial X^A}, \quad \mathbf{g}_a \equiv \frac{\partial}{\partial x^a}.$$
 (8)

Corresponding dual bases cotangent to  $B_{\text{ref}}$  and  $B_{\text{cur}}$ , respectively, are written as  $\mathbf{G}^A$  and  $\mathbf{g}^a$ , and are defined such that the following dual (i.e., scalar) products are satisfied:

$$\langle \mathbf{G}^A, \mathbf{G}_B \rangle = \delta_B^A, \quad \langle \mathbf{g}^a, \mathbf{g}_b \rangle = \delta_b^a,$$
 (9)

where  $\delta_B^A$  and  $\delta_b^a$  are Kronecker's delta symbols, i.e.  $\delta_B^A = 1$  for A = B,  $\delta_B^A = 0$  for  $A \neq B$ , with analogous relations for  $\delta_b^a$ . From (8) we see that the basis vectors of the Euclidean spaces  $B_{\text{ref}}$  and  $B_{\text{cur}}$  are *holonomic basis vectors*, satisfying the integrability conditions [13]

$$\mathbf{G}_{[A,B]} = \mathbf{0}, \quad \mathbf{g}_{[a,b]} = \mathbf{0}.$$
 (10)

The deformation gradient is then written as follows in terms of components and basis vectors:

$$\mathbf{F} = F_{A}^{a} \mathbf{g}_{a} \otimes \mathbf{G}^{A} = \frac{\partial x^{a}}{\partial X^{A}} \mathbf{g}_{a} \otimes \mathbf{G}^{A}. \tag{11}$$

Similarly, we write for  $F^e$  and  $F^p$ :

$$\mathbf{F}^{\mathbf{p}} = F_{A}^{\mathbf{p}^{\alpha}} \tilde{\mathbf{g}}_{\alpha} \otimes \mathbf{G}^{A}, \quad \mathbf{F}^{\mathbf{e}} = F_{\alpha}^{\mathbf{e}^{a}} \mathbf{g}_{a} \otimes \tilde{\mathbf{g}}^{\alpha}, \tag{12}$$

where the *anholonomic basis vectors*  $\tilde{\mathbf{g}}_{\alpha}$  and associated covectors  $\tilde{\mathbf{g}}^{\alpha}$  must obey

$$\langle \tilde{\mathbf{g}}^{\alpha}, \tilde{\mathbf{g}}_{\beta} \rangle = \delta_{\beta}^{\alpha} \tag{13}$$

in order to ensure satisfaction of the multiplicative decomposition (1), and where  $\delta^{\alpha}_{\beta} = 1$  for  $\alpha = \beta$  and  $\delta^{\alpha}_{\beta} = 0$  for  $\alpha \neq \beta$ . In general,  $\tilde{\mathbf{g}}_{[\alpha,\beta]} \neq \mathbf{0}$  (compare with Eq. (10) for holonomic bases), since we cannot differentiate with respect to *anholonomic coordinates*  $\tilde{x}^{\alpha} \in \tilde{B}_{int}$  in the conventional manner and since no relations analogous to (8) apply to the  $\tilde{\mathbf{g}}_{\alpha}$ . If we *define* anholonomic coordinate differentiation as [13]

$$\frac{\partial()}{\partial \tilde{x}^{\alpha}} \equiv \frac{\partial()}{\partial X^{A}} F_{,\alpha}^{p-1^{A}} = \frac{\partial()}{\partial x^{a}} F_{,\alpha}^{e^{a}}, \tag{14}$$

then

$$\tilde{\mathbf{g}}_{[\alpha,\beta]} = \tilde{\mathbf{g}}_{[\alpha,A} F_{.\beta]}^{p-1^{A}} = \tilde{\mathbf{g}}_{[\alpha,a} F_{.\beta]}^{e^{a}} \neq 0$$
(15)

are additional conditions associated with the anholonomicity of configuration  $\tilde{B}_{int}$ . On the other hand, *only* when  $\tilde{B}_{int}$  is simply connected (and Euclidean), meaning that the  $\tilde{x}^{\alpha}$  are holonomic coordinates of  $x^{a}$  or  $X^{A}$ , do we have

$$F_{A}^{\mathbf{p}^{\alpha}} = \frac{\partial \tilde{\mathbf{x}}^{\alpha}}{\partial X^{A}}, \quad F_{a}^{\mathbf{e}-1^{\alpha}} = \frac{\partial \tilde{\mathbf{x}}^{\alpha}}{\partial x^{a}}, \quad \tilde{\mathbf{g}}_{\alpha} = \frac{\partial}{\partial \tilde{\mathbf{x}}^{\alpha}},$$
$$\tilde{\mathbf{g}}_{[\alpha,\beta]} = \mathbf{0}. \tag{16}$$

#### 3. The metric tensor on an anholonomic space

The metric tensor on the anholonomic space  $\tilde{B}_{int}$  is written here as  $\tilde{\mathbf{g}} = \tilde{g}_{\alpha\beta}\tilde{\mathbf{g}}^{\alpha} \otimes \tilde{\mathbf{g}}^{\beta}$  and is symmetric by definition, i.e.  $\tilde{g}_{\alpha\beta} = \tilde{g}_{\beta\alpha}$ . It satisfies

$$\tilde{g}_{\alpha\beta} = \tilde{\mathbf{g}}_{\alpha} \cdot \tilde{\mathbf{g}}_{\beta},\tag{17}$$

where "·" denotes the scalar product or inner product of contravariant vectors. The scalar product of two arbitrary vectors  $\tilde{\mathbf{a}}$  and  $\tilde{\mathbf{b}}$  on the tangent space of  $\tilde{B}_{\text{int}}$  then becomes, from (17),

$$\tilde{\mathbf{a}} \cdot \tilde{\mathbf{b}} = \tilde{a}^{\alpha} \tilde{\mathbf{g}}_{\alpha} \cdot \tilde{b}^{\beta} \tilde{\mathbf{g}}_{\beta} = \tilde{a}^{\alpha} \tilde{b}^{\beta} (\tilde{\mathbf{g}}_{\alpha} \cdot \tilde{\mathbf{g}}_{\beta}) = \tilde{a}^{\alpha} \tilde{g}_{\alpha\beta} \tilde{b}^{\beta}.$$
(18)

Components of the metric tensor  $\tilde{\mathbf{g}}$  are used to lower indices in the conventional manner, i.e.,

$$\tilde{a}_{\alpha} = \tilde{g}_{\alpha\beta}\tilde{a}^{\beta},\tag{19}$$

and are needed to compute the transpose maps of mixed-variant tensors (cf. [15]), e.g.,

$$F_{.a}^{eT^{\alpha}} = \tilde{g}^{\alpha\beta} F_{.\beta}^{e^{b}} g_{ab} = \tilde{g}^{\alpha\beta} F_{\beta}^{e^{*}b} g_{ba},$$

$$F_{,\alpha}^{\mathbf{p}T^{A}} = \tilde{g}_{\alpha\beta}F_{B}^{\mathbf{p}^{\beta}}G^{AB} = \tilde{g}_{\alpha\beta}F_{B}^{\mathbf{p}^{*},\beta}G^{BA},\tag{20}$$

where  $\tilde{g}^{\alpha\beta}$  are components of the inverse metric  $\tilde{\mathbf{g}}^{-1}$ ,  $G^{AB}$  are components of the inverse of the metric tensor  $\mathbf{G}$  on the reference configuration  $B_{\text{ref}}$ , and  $g_{ab}$  are components of the metric tensor  $\mathbf{g}$  on  $B_{\text{cur}}$ . Additionally in (20) the dual map operation corresponding to a horizontal exchange of indices is denoted by the superposed "\*" [24,25]. From relations (20), we are in position to define symmetric elastic and plastic strain tensors referred to the current and reference configurations, respectively, e.g. the covariant  $\mathbf{C}^{\text{e}}$  and  $\mathbf{C}^{\text{p}}$ :

$$C_{ab}^{e} \equiv F_{.a}^{eT^{\alpha}} g_{bc} F_{.\alpha}^{e^{c}} = C_{ba}^{e},$$

$$C_{AB}^{p} \equiv F_{\alpha}^{pT^{c}} G_{CA} F_{\alpha}^{p} = C_{BA}^{p}.$$
(21)

The metric tensor  $\tilde{\mathbf{g}}$  is also needed to symmetrize nominally mixed-variant tensors referred to configuration  $\tilde{B}_{\text{int}}$ . For example, consider the so-called "plastic velocity gradient"  $\hat{\mathbf{L}}^p$ :

$$\tilde{\mathbf{L}}^{p} \equiv \dot{\mathbf{F}}^{p} \mathbf{F}^{p-1}, \quad \tilde{L}_{.\beta}^{p^{\alpha}} \equiv \dot{F}_{.A}^{p^{\alpha}} F_{.\beta}^{p-1}, \tag{22}$$

where the superposed dot denotes the material time derivative. The transpose of the *covariant* version of  $\tilde{\mathbf{L}}^p$  is written

$$\tilde{L}_{\alpha\beta}^{pT} = \tilde{L}_{\beta\alpha}^{p} = \tilde{g}_{\beta\gamma}\dot{F}_{.\alpha}^{p^{\gamma}}F_{.\alpha}^{p-1}$$
(23)

from which follow the *covariant* symmetric rate of plastic deformation  $\tilde{\mathbf{D}}^p$  and the skew-symmetric "plastic spin"  $\tilde{\mathbf{W}}^p$ :

$$\begin{split} 2\tilde{D}^{\rm p}_{\alpha\beta} &= \tilde{L}^{\rm p}_{\alpha\beta} + \tilde{L}^{\rm p}_{\beta\alpha}, \quad 2\tilde{W}^{\rm p}_{\alpha\beta} = \tilde{L}^{\rm p}_{\alpha\beta} - \tilde{L}^{\rm p}_{\beta\alpha}, \\ \tilde{L}^{\rm p}_{\alpha\beta} &= \tilde{D}^{\rm p}_{\alpha\beta} + \tilde{W}^{\rm p}_{\alpha\beta}. \end{split} \tag{24}$$

Multiplying (24) by through by  $\tilde{q}^{\alpha\beta}$  results in

$$\tilde{L}_{\beta}^{p^{\alpha}} = \tilde{g}^{\alpha \chi} \tilde{D}_{\gamma \beta}^{p} + \tilde{g}^{\alpha \chi} \tilde{W}_{\gamma \beta}^{p} = \tilde{D}_{\beta}^{p^{\alpha}} + \tilde{W}_{\beta}^{p^{\alpha}}, \tag{25}$$

where  $\tilde{D}^{p^z}_{.\beta} \equiv \tilde{g}^{\alpha\chi}\tilde{D}^p_{\chi\beta}$  and  $\tilde{W}^{p^z}_{.\beta} \equiv \tilde{g}^{\alpha\chi}\tilde{W}^p_{\chi\beta}$  both depend upon the metric  $\tilde{\mathbf{g}}$  (from (23)) and its inverse (from

(25)). We thus see that the plastic velocity gradient  $\tilde{\mathbf{L}}^p$  can only be decomposed into stretch rate and spin terms after a metric tensor  $\tilde{\mathbf{g}}$  has been introduced, as noted by Maugin [18].

Jacobian invariants of deformation mappings  $\mathbf{F}^{\mathrm{e}}$  and  $\mathbf{F}^{\mathrm{p}}$  defining the relationships between volume elements  $\mathrm{d}v \subset B_{\mathrm{cur}}$ ,  $\mathrm{d}\tilde{v} \subset \tilde{B}_{\mathrm{int}}$ , and  $\mathrm{d}V \subset B_{\mathrm{ref}}$  also depend upon  $\tilde{\mathbf{g}}$ . For example, letting  $\tilde{z}^{\alpha}$  and  $Z^A$  denote coordinates referred to local Cartesian frames on  $\tilde{B}_{\mathrm{int}}$  and  $B_{\mathrm{ref}}$ , respectively, we write [8]

$$J^{p} \equiv \frac{\mathrm{d}\tilde{v}}{\mathrm{d}V} = \det\left(\frac{\partial \tilde{z}^{\alpha}}{\partial Z^{A}}\right) = \det\left(\frac{\partial \tilde{z}^{\alpha}}{\partial \tilde{x}^{\beta}}F_{.B}^{p^{\beta}}\frac{\partial X^{B}}{\partial Z^{A}}\right)$$
$$= \det(F_{.B}^{p^{\beta}})\sqrt{\det(\tilde{g}_{\alpha\beta})/\det(G_{AB})},\tag{26}$$

where we have used the identities  $\det(\tilde{g}_{\alpha\beta}) = (\det(\partial \tilde{z}^{\alpha}/\partial \tilde{x}^{\beta}))^2$  and  $\det(G_{AB}) = (\det(\partial Z^A/\partial X^B))^2$  (cf. [15]). Analogously for  $\mathbf{F}^e$  we write

$$J^{e} \equiv \frac{\mathrm{d}v}{\mathrm{d}\tilde{v}} = \det\left(\frac{\partial z^{a}}{\partial \tilde{z}^{\alpha}}\right) = \det\left(\frac{\partial z^{a}}{\partial x^{b}}F^{e_{,\beta}^{b}}\frac{\partial \tilde{x}^{\beta}}{\partial \tilde{z}^{\alpha}}\right)$$
$$= \det(F^{e_{,\beta}^{b}})\sqrt{\det(g_{ab})/\det(\tilde{g}_{\alpha\beta})},\tag{27}$$

with  $z^a$  denoting Cartesian coordinates on  $B_{\text{cur}}$  such that  $\det(g_{ab}) = (\det(\partial z^a/\partial x^b))^2$ . We can alternatively write (26) and (27) as [26]

$$J^{p} = \frac{1}{6} \tilde{\varepsilon}_{\alpha\beta\chi} \varepsilon^{ABC} F_{.A}^{p^{\alpha}} F_{.B}^{p^{\beta}} F_{.C}^{p^{\alpha}}$$
$$= \frac{1}{6} (\sqrt{\tilde{g}/G}) e_{\alpha\beta\chi} e^{ABC} F_{.A}^{p^{\alpha}} F_{.B}^{p^{\beta}} F_{.C}^{p^{\alpha}}, \tag{28}$$

$$J^{e} = \frac{1}{6} \hat{\epsilon}^{\alpha\beta\chi} \epsilon_{abc} F^{e^{a}}_{,\alpha} F^{e^{b}}_{,\beta} F^{e^{c}}_{,\chi}$$
$$= \frac{1}{6} (\sqrt{g/\tilde{g}}) e^{\alpha\beta\chi} e_{abc} F^{e^{a}}_{,\alpha} F^{e^{b}}_{,\beta} F^{e^{c}}_{,\chi}, \tag{29}$$

where we have used the shorthand notation  $g \equiv \det(g_{ab})$ ,  $\tilde{g} \equiv \det(\tilde{g}_{\alpha\beta})$ , and  $G \equiv \det(G_{AB})$ . Permutation tensors in Eqs. (28) and (29) are defined by  $\varepsilon^{ABC} \equiv \sqrt[-1]{G}e^{ABC}$ ,  $\tilde{\varepsilon}_{\alpha\beta\chi} \equiv \sqrt{\tilde{g}}e_{\alpha\beta\chi}$ ,  $\varepsilon_{abc} \equiv \sqrt{g}e_{abc}$ , and  $\tilde{\varepsilon}^{\alpha\beta\chi} \equiv \sqrt[-1]{\tilde{g}}e^{\alpha\beta\chi}$ , with  $e^{ABC}$ ,  $e_{\alpha\beta\chi}$ ,  $e_{abc}$ , and  $e^{\alpha\beta\chi}$  standard permutation symbols each referred to the configuration indicated by its indices. Consider for example the incompatibility described by Eq. (5), which can be rewritten as

$$\tilde{b}^{\alpha} = -\int_{a} F_{.[a,b]}^{e-1^{\alpha}} dx^{a} \wedge dx^{b} = -\int_{a} \varepsilon^{abc} F_{.[a,b]}^{e-1^{\alpha}} n_{c} da$$

$$= -\int_{a} \varepsilon^{abc} F_{.a,b}^{e-1^{\alpha}} n_{c} da = \int_{a} A^{e^{\alpha c}} n_{c} da, \qquad (30)$$

where the second rank area element has been converted to an axial covector  $\mathbf{n} da$  via  $dx^a \wedge dx^b = \varepsilon^{abc} n_c da$ , and where the two-point dislocation density tensor  $A^{e^{ac}} \equiv -\varepsilon^{abc} F^{e-1^a}_{a,b}$ . Mapping the integrand in (30) to the intermediate configuration via Nanson's formula (cf. [27]) gives

$$\tilde{b}^{\alpha} = \int_{a} A^{e^{\alpha c}} n_{c} da = \int_{\tilde{a}} J^{e} F_{.c}^{e-1} A^{e^{\alpha c}} \tilde{n}_{\beta} d\tilde{a}$$

$$= \int_{\tilde{a}} \tilde{A}^{e^{\beta c}} \tilde{n}_{\beta} d\tilde{a}, \qquad (31)$$

where  $\tilde{A}^{e^{\beta z}} \equiv J^e F_{.c}^{e-1^{\beta}} A^{e^{zc}}$  is the intermediate configuration dislocation density tensor, which depends upon  $J^e$  and hence, from Eq. (29),  $\tilde{g}$ . Should we opt to allow the (scalar) residual free energy  $\tilde{\psi}^{\text{GN}}$  of the crystal associated with geometrically necessary dislocations to depend quadratically upon a dislocation density measure referred to  $\tilde{B}_{\text{int}}$  such as  $\tilde{\mathbf{A}}^e$  (cf. [27–29]), we then write, for example,

$$\tilde{\psi}^{\text{GN}} = \frac{1}{2}\mu l^2 \tilde{\mathbf{A}}^{\text{e}} : \tilde{\mathbf{A}}^{\text{e}} = \frac{1}{2}\mu l^2 \tilde{A}^{e^{\alpha\beta}} \tilde{g}_{\alpha\alpha} \tilde{g}_{\beta\delta} \tilde{A}^{e^{\alpha\delta}}, \tag{32}$$

where  $\mu$  and l are an elastic shear modulus and characteristic length, respectively. Thus, the scalar product in Eq. (32) is another instance in finite crystalline elastoplasticity where  $\tilde{\mathbf{g}}$  is required.

# 4. Metric tensors and anholonomic basis vectors: possible choices

We now discuss some conceivable choices for the metric tensor  $\tilde{\mathbf{g}}$  and associated basis vectors  $\tilde{\mathbf{g}}_{\alpha}$ . The simplest and by far most prevalent option from the literature is to impose (cf. [7,8,22,30])

$$\tilde{g}_{\alpha\beta} = \tilde{\mathbf{g}}_{\alpha} \cdot \tilde{\mathbf{g}}_{\beta} = \delta_{\alpha\beta},\tag{33}$$

with  $\delta_{\alpha\beta}$  the covariant Kronecker's delta, i.e.  $\delta_{\alpha\beta}=1$  for  $\alpha=\beta$  and  $\delta_{\alpha\beta}=0$  for  $\alpha\neq\beta$ . Eq. (33) indicates that contravariant vectors defined on  $\tilde{B}_{\rm int}$  are referred to a single global Cartesian frame (i.e., orthonormal  $\tilde{\mathbf{g}}_{\alpha}$ ), or, equivalently, a parallel (i.e., identical) Cartesian frame attached to each local relaxed volume element  $\mathrm{d}\tilde{v}\subset\tilde{B}_{\rm int}$ . Such a choice implies either that (i)  $\tilde{B}_{\rm int}$  is a Euclidean space or that (ii) the  $\tilde{\mathbf{g}}_{\alpha}$  are not actually tangent to any coordinate lines scribed on the base manifold  $\tilde{B}_{\rm int}$  (since such coordinates do not exist in the

discontinuous anholonomic space) but instead correspond to some external reference frame. As discussed already in Section 2 of the present work, statement (i) is ruled out in the presence of crystal defects such as dislocations that render  $B_{int}$  anholonomic. This leaves statement (ii), which is difficult to interpret geometrically: from its standpoint, vectors in configuration  $\tilde{B}_{\mathrm{int}}$  are not referred to the actual tangent spaces of a material manifold in  $\tilde{B}_{int}$  but are instead referred to the fixed external Cartesian frame(s). The intermediate metric  $\delta_{\alpha\beta}$  (or equivalently, the external Cartesian frame) is introduced rather artificially in such theories as an additional constitutive entity, accompanying variables F<sup>e</sup> and F<sup>p</sup>. We also mention the related work of Simo [31], wherein the intermediate configuration metric is given by  $\tilde{g}_{\alpha\beta} = \delta^{A}_{.\alpha} G_{AB} \delta^{B}_{.\beta}$ , implying a Euclidean metric structure for  $\tilde{B}_{int}$  when  $B_{ref}$  is Euclidean, and relying upon the external two-point construct  $\delta_{\alpha}^{A}$ . While we are unable to rigorously rule out the choice (33) on any fundamental grounds, we emphasize next several alternatives that have been proposed in the literature that, in contrast to Eq. (33), do not make the embedding of a non-Euclidean space  $\tilde{B}_{int}$  within a global Cartesian space equipped with a Euclidean metric tensor  $\delta_{\alpha\beta}$ . (It should be noted, however, that our derivations (26) and (27), wherein Cartesian  $\tilde{z}^{\alpha}$ are assigned to each volume element  $d\tilde{v} \subset \tilde{B}_{int}$ , do rely on such an assumption, at least locally.)

One such alternative is to specify the metric tensor  $\tilde{\mathbf{g}}$  as the covariant elastic deformation tensor  $\tilde{\mathbf{C}}^{e}$  [17,18,20], i.e.

$$\tilde{g}_{\alpha\beta} = \tilde{C}^{e}_{\alpha\beta} \equiv F^{e^{a}}_{\alpha} g_{ab} F^{e^{b}}_{.\beta} = F^{e^{a}}_{\alpha} \mathbf{g}_{a} \cdot F^{e^{b}}_{.\beta} \mathbf{g}_{b} = \tilde{\mathbf{g}}_{\alpha} \cdot \tilde{\mathbf{g}}_{\beta},$$
(34)

implying that the anholonomic basis vectors are defined by  $\tilde{\mathbf{g}}_{\alpha} \equiv F_{\alpha}^{e^a} \mathbf{g}_a$ . Analogously, one could implement the covariant plastic deformation tensor  $\tilde{\mathbf{C}}^p$  as a metric [32]

$$\tilde{g}_{\alpha\beta} = \tilde{C}_{\alpha\beta}^{p} \equiv F_{,\alpha}^{p-1^{A}} G_{AB} F_{,\beta}^{p-1^{B}}$$

$$= F_{,\alpha}^{p-1^{A}} \mathbf{G}_{A} \cdot F_{,\beta}^{p-1^{B}} \mathbf{G}_{B} = \tilde{\mathbf{g}}_{\alpha} \cdot \tilde{\mathbf{g}}_{\beta}, \tag{35}$$

meaning that  $\tilde{\mathbf{g}}_{\alpha} \equiv F_{.\alpha}^{p-1^A} \mathbf{G}_A$ . (It should be noted that Miehe [32] suggested several alternative metric tensors on each configuration, in addition to (35).) In Eqs. (34) and (35) we have used, respectively, the standard Euclidean relations  $g_{ab} = \mathbf{g}_a \cdot \mathbf{g}_b$  and  $G_{AB} = \mathbf{G}_A \cdot \mathbf{G}_B$ . The  $\tilde{\mathbf{g}}_{\alpha}$  in (34) or (35) are still not tangent to any global

coordinate curves  $\tilde{x}^{\alpha}$  (since such coordinates are precluded by the anholonomicity of  $\tilde{B}_{int}$ ), but they do exist in a one-to-one manner with the set  $\mathbf{g}_a(\mathbf{x})$  and the map  $\mathbf{F}^e$  or with the set  $\mathbf{G}_A(\mathbf{X})$  and the map  $\mathbf{F}^{p-1}$ , respectively. It follows that  $\tilde{\mathbf{C}}^e$  and  $\tilde{\mathbf{C}}^p$  are well-defined geometric quantities referred to the space  $\tilde{B}_{int}$ , in contrast to the somewhat artificial, external object  $\delta_{\alpha\beta}$  of (33) that cannot be derived from the elastic or plastic tangent maps and basis vectors on  $B_{ref}$  or  $B_{cur}$ . Consider now the rank 4 Riemann–Christoffel curvature tensor formed from  $\tilde{\mathbf{C}}^e$  on the anholonomic space  $\tilde{B}_{int}$ , with components [13,14]

$$\begin{split} \tilde{R}^{\alpha}_{\beta\chi\delta} &\equiv \frac{\partial \tilde{\Gamma}^{\alpha}_{\delta\beta}}{\partial \tilde{x}^{\chi}} - \frac{\partial \tilde{\Gamma}^{\alpha}_{\chi\beta}}{\partial \tilde{x}^{\delta}} + \tilde{\Gamma}^{\alpha}_{\chi\epsilon} \tilde{\Gamma}^{\epsilon}_{\delta\beta} \\ &- \tilde{\Gamma}^{\alpha}_{\delta\epsilon} \tilde{\Gamma}^{\epsilon}_{\gamma\beta} + 2 \tilde{\kappa}^{\epsilon}_{\gamma\delta} \tilde{\Gamma}^{\alpha}_{\epsilon\beta}, \end{split} \tag{36}$$

where the coefficients of the metric connection are found by  $2\tilde{C}_{\alpha\beta}^{\rm e}\tilde{\Gamma}_{\delta\chi}^{\rm e}=\tilde{C}_{\chi\beta,\delta}^{\rm e}+\tilde{C}_{\delta\beta,\chi}^{\rm e}-\tilde{C}_{\delta\chi,\beta}^{\rm e}$  and components of the anholonomic object by  $\tilde{\kappa}_{\chi\delta}^{\rm e}=F_{,\chi}^{\rm e}F_{,\delta}^{\rm e}F_{,[a,b]}^{\rm e-1^{\rm e}}$ . The conditions  $\tilde{R}_{\beta\chi\delta}^{\rm e}=0$  and  $\tilde{\kappa}_{\chi\delta}^{\rm e}=0$  hold identically only when  $F_{,\alpha}^{\rm ea}=x_{,\alpha}^{a}$ , i.e., only when  $\tilde{B}_{\rm int}$  is homeomorphic to the Euclidean space  $B_{\rm cur}$  and  $\tilde{x}^{\alpha}$  are holonomic coordinates for which we can define partial differentiation as usual. Under such conditions,  $\tilde{R}_{\beta\chi\delta}^{\alpha}$  is the pull-back of the curvature tensor formed from the metric tensor  $g_{ab}$ , which itself vanishes since  $B_{\rm cur}$  is Euclidean. Analogous statements regarding the curvature can be made for  $\tilde{\bf C}^{\rm p}$ , i.e. the curvature tensor derived from  $\tilde{\bf C}^{\rm p}$  vanishes identically only when  $F_{,A}^{\rm pa}=\tilde{x}_{,A}^{\alpha}$  and  $\tilde{B}_{\rm int}$  is Euclidean.

A third alternative methodology [33] involves introduction of the new multiplicative decomposition

$$\mathbf{F} = \hat{\mathbf{F}}^{e} \hat{\mathbf{F}}^{p}, \quad F_{A}^{a} = \hat{F}_{B}^{e^{a}} \hat{F}_{A}^{p^{B}}, \tag{37}$$

where both legs of the new plastic deformation tensor  $\hat{\mathbf{F}}^p$  are referred to  $B_{\text{ref}}$  and where  $\hat{\mathbf{F}}^e$  is a two-point tensor between tangent spaces of  $B_{\text{ref}}$  and  $B_{\text{cur}}$ , i.e.

$$\hat{\mathbf{F}}^{e} = \hat{F}_{B}^{e^{a}} \mathbf{g}_{a} \otimes \mathbf{G}^{B}, \quad \hat{\mathbf{F}}^{p} = \hat{F}_{A}^{p^{B}} \mathbf{G}_{B} \otimes \mathbf{G}^{A}. \tag{38}$$

Following Le and Stumpf [33], we introduce the two-point transformation matrix **H**, satisfying

$$F_{,\alpha}^{e^a} = \hat{F}_{,B}^{e^a} H_{,\alpha}^{-1^B}, \quad F_{,A}^{p^\alpha} = H_{,B}^{\alpha} \hat{F}_{,A}^{p^B},$$
 (39)

such that Eqs. (1) and (37) are satisfied simultaneously

$$F_{A}^{a} = F_{A}^{e^{a}} F_{A}^{p^{\alpha}} = \hat{F}_{B}^{e^{a}} H_{A}^{-1^{B}} H_{B}^{\alpha} \hat{F}_{A}^{p^{B}} = \hat{F}_{B}^{e^{a}} \hat{F}_{A}^{p^{B}}.$$
 (40)

The anholonomic basis vectors and covectors are found in terms of **H** as, respectively,

$$\tilde{\mathbf{g}}_{\alpha} \equiv H_{,\alpha}^{-1^A} \mathbf{G}_A, \quad \tilde{\mathbf{g}}^{\alpha} \equiv H_{,A}^{\alpha} \mathbf{G}^A,$$
 (41)

so that the dual product obeys the standard relations

$$\langle \tilde{\mathbf{g}}_{\alpha}, \tilde{\mathbf{g}}^{\beta} \rangle = \langle H_{.\alpha}^{-1} \mathbf{G}_{A}, H_{.B}^{\beta} \mathbf{G}^{B} \rangle = H_{.\alpha}^{-1} H_{.B}^{\beta} \langle \mathbf{G}_{A}, \mathbf{G}^{B} \rangle$$
$$= H_{.\alpha}^{-1} H_{.B}^{\beta} \delta_{A}^{B} = \delta_{\alpha}^{\beta}, \tag{42}$$

leading then to the representation of the metric tensor on  $\tilde{B}_{\rm int}$ :

$$\tilde{g}_{\alpha\beta} = \tilde{\mathbf{g}}_{\alpha} \cdot \tilde{\mathbf{g}}_{\beta} = H_{,\alpha}^{-1^{A}} \mathbf{G}_{A} \cdot H_{,\beta}^{-1^{B}} \mathbf{G}_{B}$$

$$= H_{,\alpha}^{-1^{A}} G_{AB} H_{,\beta}^{-1^{B}}.$$
(43)

Eq. (41) implies that the elastic deformation maps  $\mathbf{F}^e$  and  $\hat{\mathbf{F}}^e$  are the same (two-point) tensor, although each is referred to different coordinate bases:

$$\mathbf{F}^{e} = F^{e^{a}}_{,\alpha} \mathbf{g}_{a} \otimes \tilde{\mathbf{g}}^{\alpha} = (\hat{F}^{e^{a}}_{,C} H^{-1}_{,\alpha}) \mathbf{g}_{a} \otimes (H^{\alpha}_{,B} \mathbf{G}^{B})$$
$$= \hat{F}^{e^{a}}_{,B} \mathbf{g}_{a} \otimes \mathbf{G}^{B} = \hat{\mathbf{F}}^{e}. \tag{44}$$

Analogously, for the plastic tangent mappings we have

$$\mathbf{F}^{\mathbf{p}} = F_{\mathcal{A}}^{\mathbf{p}^{\alpha}} \tilde{\mathbf{g}}_{\alpha} \otimes \mathbf{G}^{A} = (\hat{F}_{\mathcal{A}}^{\mathbf{p}^{C}} H_{\mathcal{C}}^{\alpha}) (H_{\mathcal{A}}^{-1^{B}} \mathbf{G}_{B}) \otimes \mathbf{G}^{A}$$
$$= \hat{F}_{\mathcal{A}}^{\mathbf{p}^{B}} \mathbf{G}_{B} \otimes \mathbf{G}^{A} = \hat{\mathbf{F}}^{\mathbf{p}}. \tag{45}$$

From the anholonomicity conditions (15) we see that

$$\tilde{\mathbf{g}}_{[\alpha,\beta]} = H_{\cdot[\alpha,\beta]}^{-1^{A}} \mathbf{G}_{A} + H_{\cdot[\alpha}^{-1^{A}} \mathbf{G}_{A,\beta]} = H_{\cdot[\alpha,\beta]}^{-1^{A}} \mathbf{G}_{A}$$

$$+ H_{\cdot[\alpha}^{-1^{A}} \mathbf{G}_{A,B} F_{\cdot\beta]}^{p-1^{B}} \neq \mathbf{0}.$$
(46)

Upon choosing a Cartesian reference coordinate system for the Euclidean space  $B_{\text{ref}}$ , we obtain  $G_{A,B} = 0$ , and Eq. (46) becomes

$$\tilde{\mathbf{g}}_{[\alpha,\beta]} = H_{\cdot[\alpha,\beta]}^{-1^A} \mathbf{G}_A \neq \mathbf{0} \to H_{\cdot[\alpha,\beta]}^{-1^A} \neq 0, \tag{47}$$

meaning that **H** (or its inverse) is generally not derivable as the gradient of a vector-valued function when  $\tilde{B}_{int}$  is anholonomic. On the other hand, *only when the intermediate configuration is holonomic* and  $\tilde{\mathbf{g}}_{[\alpha,\beta]} = \mathbf{0}$  can we write

$$H_A^{\alpha} = \frac{\partial \tilde{y}^{\alpha}}{\partial X^A}, \quad H_{\alpha}^{-1^A} = \frac{\partial X^A}{\partial \tilde{v}^{\alpha}},$$
 (48)

where  $\tilde{y}^{\alpha} = \tilde{y}^{\alpha}(X^A, t)$  are new coordinate functions on  $\tilde{B}_{int}$ , not necessarily identical to  $\tilde{x}^{\alpha}$ . Upon invocation of the holonomicity relations (16) we obtain

$$\hat{F}_{A}^{e^{a}} = F_{\alpha}^{e^{a}} \frac{\partial \tilde{y}^{\alpha}}{\partial X^{A}} = \frac{\partial x^{a}}{\partial \tilde{x}^{\alpha}} \frac{\partial \tilde{y}^{\alpha}}{\partial X^{A}},$$

$$\hat{F}_{A}^{p^{B}} = \frac{\partial X^{B}}{\partial \tilde{y}^{\alpha}} F_{A}^{p^{\alpha}} = \frac{\partial X^{B}}{\partial \tilde{y}^{\alpha}} \frac{\partial \tilde{x}^{\alpha}}{\partial X^{A}},$$
(49)

from which, for the particular choice of  $\tilde{x}^{\alpha} = \tilde{y}^{\alpha}$ , results in  $\hat{F}^{\mathrm{e}_{A}^{a}} = F_{A}^{a}$  and  $\hat{F}_{A}^{\mathrm{p}_{B}^{B}} = \delta_{A}^{B}$ . Returning now to the anholonomic case and substituting (39) into (4), we see that the incompatibility (i.e., closure failure or net Burgers vector in configuration  $\tilde{B}_{\mathrm{int}}$ ) depends simultaneously upon gradients of  $\hat{F}_{A}^{p}$  and  $H_{C}^{\alpha}$ :

$$\tilde{b}^{\alpha} = -\int_{A} (H\hat{F}^{p})_{.[A,B]}^{\alpha} dX^{A} \wedge dX^{B}$$

$$= -\int_{A} (\hat{F}_{.[A,B]}^{p^{C}} H_{.C}^{\alpha} + \hat{F}_{.[A}^{p^{C}} H_{.C,B]}^{\alpha}) dX^{A} \wedge dX^{B}, \quad (50)$$

implying that knowledge of components and gradients of  $\hat{F}_{A}^{p^{B}}$  alone is not sufficient to characterize the incompatibility of Eq. (4) (i.e., one needs either  $F_{\perp}^{p^{\alpha}}$  $(\text{Eq.}(4)), F_{a}^{e-1^{\alpha}}(\text{Eq.}(5)), \text{ or } both \text{ of } \hat{F}_{A}^{p^{B}} \text{ and } H_{B}^{\alpha}(\text{Eq.}(5))$ (50)). Thus, while attractive at first glance since no anholonomic basis vectors directly enter the multiplicative decomposition (37), the methodology outlined in Eqs. (37)–(50) can only be used within the context of classical higher-order gradient, dislocation-based crystalline elastoplasticity, wherein the incompatibility is referred to the anholonomic intermediate configuration  $\tilde{B}_{int}$ , when the additional tensor **H** and its inverse are available for mapping to and from that configuration. However, the method should definitely not be disregarded, as Le and Stumpf [33] successfully applied this description to define a different Burgers vector **B** (i.e., an incompatibility) referred to the holonomic reference configuration, in terms of the lack of integrability of  $\hat{\mathbf{F}}^{e}$ , i.e.

$$B^{A} \equiv \oint_{c} \hat{F}_{.a}^{e-1^{A}} dx^{a} = -\int_{a} \hat{F}_{.[a,b]}^{e-1^{A}} dx^{a} \wedge dx^{b}.$$
 (51)

It should be noted that in this context, components of  $\hat{F}_{\mathcal{A}}^{e^a}$  are not associated with loading from a locally unstressed and anholonomic state to a stressed state, but rather describe, at each point in the crystal, the stretch and rotation of a triad of lattice director vectors occurring between the initial configuration and the current

configuration, with  $\hat{\mathbf{F}}^p = \hat{\mathbf{F}}^{e-1}\mathbf{F}$  any remaining "inelastic" deformation referred to the reference state.

#### 5. Discussion

Additional critical comments regarding the particular choices of intermediate configuration metric tensor listed in Eqs. (33), (34), (35), and (43) are now in order. Consider first the designation given by (33):  $\tilde{g}_{\alpha\beta} = \delta_{\alpha\beta}$ . This prescription is by far the most common in finite deformation plasticity theories from the literature, as it is made implicitly whenever Cartesian coordinates for the intermediate configuration  $\tilde{B}_{int}$  are invoked, be it for the purpose of defining differential volume change [7,8], calculating a norm or scalar product of contravariant vectors or tensors [27–30], or decomposing the plastic velocity gradient  $\tilde{\mathbf{L}}^p$  into distinct deformation rate and spin terms (cf. [34]). We remark that Regueiro et al. [29] acknowledged the non-Euclidean character of  $\tilde{B}_{int}$  but gave no explicit alternative to the Cartesian metric tensor for use on  $\tilde{B}_{int}$ . As stated already, choice (33) cannot be ruled out unequivocally via mathematical or physical arguments. However, since the unit metric tensor (i.e., covariant Kronecker's delta  $\delta_{\alpha\beta}$ ) is not considered a well-defined geometric variable on a non-Euclidean space (cf. [16]), and since  $\tilde{B}_{int}$ is clearly non-Euclidean (i.e., not homeomorphic to three-dimensional Euclidean space) under conditions of heterogeneous, incompatible plastic deformation, the metric  $\delta_{\alpha\beta}$  of (33) must be viewed as an additional, stationary constitutive variable introduced by the modeler, accompanying any constitutive relations specifying the time evolution of components of F<sup>e</sup> and  $\mathbf{F}^p$ . In contrast, the choices given in (34), (35), and (43)—wherein the intermediate metric tensors are defined directly in terms of elastic or inelastic tangent mappings—may be viewed as favorable alternatives to (33) since the former do not require the modeler to prescribe an intermediate metric via introduction of an additional constitutive variable. Maugin [19] voiced similar opinions regarding the choice of metric tensor on our natural configuration B (Fig. 1), cautioning against usage of a Cartesian metric on a non-Euclidean space. Instead, Maugin [19] elected to employ the quantity  $\mathscr{K}^a_{.a}g_{ab}\mathscr{K}^b_{.\ell}$  as a metric for lowering contravariant indices on the generally

anholonomic space  $\mathscr{B}$ . It should also be noted that while the *covariant* object  $\delta_{\alpha\beta}$  cannot be constructed directly from anholonomic mappings  $\mathbf{F}^{\mathrm{e}}$  or  $\mathbf{F}^{\mathrm{p}}$ , the *mixed-variant* unit tensor (i.e., *true* Kronecker's delta)  $\delta^{\alpha}_{.\beta}$  can be introduced explicitly via the inverse operation, i.e.  $\delta^{\alpha}_{.\beta} = F^{\mathrm{e}^{-1^{\alpha}}}_{.a} F^{\mathrm{e}^{a}}_{.\beta}$  or  $\delta^{\alpha}_{.\beta} = F^{\mathrm{p}^{\alpha}}_{.\beta} F^{\mathrm{p}^{-1^{A}}}_{.\beta}$ .

Eq. (34), prescribing  $\tilde{g}_{\alpha\beta} = \tilde{C}^{e}_{\alpha\beta} \equiv F^{e^a}_{\alpha} g_{ab} F^{e^b}_{\beta}$  as a possible alternative to (33), has been proposed explicitly by at least several others [17,18,20], and is analogous to the aforementioned approach favored by Maugin [19] when  $\mathcal{K}$  is replaced by  $\mathbf{F}^{\mathbf{e}}$ . The quantity  $C_{\alpha\beta}^{e}$  is considered to be a well-defined geometric entity with indices referred to the intermediate configuration  $\tilde{B}_{\rm int}$ , since its constituents  $F_{\alpha}^{\rm e^a}$  and  $g_{ab}$  are by definition single-valued functions of current coordinates  $x^a$ . (This is in contrast to the external construct  $\delta_{\alpha\beta}$  which must be introduced by an additional constitutive assumption.) Moreover, the Riemann-Christoffel curvature tensor  $\tilde{R}^{\alpha}_{\beta\gamma\delta}$  and the anholonomic object  $\kappa^{\alpha}_{\beta\gamma}$  of Eq. (36) both vanish identically only when  $\mathbf{F}^{e-1}$  is an integrable function of  ${\bf x}$  and  $\tilde{B}_{\rm int}$  is Euclidean, meaning that assignment of  $\tilde{C}^{\rm e}_{\alpha\beta}$  as components of a metric tensor agrees fully with the non-Euclidean nature of the generally anholonomic space  $\tilde{B}_{int}$ . Consider also the implications of choice (34) in a thermodynamic assumption for stored elastic energy such as Eq. (32): the free energy associated with geometrically necessary dislocations, written herein as  $\tilde{\psi}^{\rm GN}$ , would depend explicitly upon the elastic strain metric  $\tilde{C}_{\alpha\beta}^{\rm e}$ . Such an assumption is in fact supported by previous physical [35] and numerical [36] experiments on various ductile pure metals and their alloys, wherein amplification of internal energy of dislocation arrays at flexing grain and sub-grain boundaries in the presence of applied loads was discovered. In light of the above reasons, we endorse here usage of  $\tilde{C}^{\rm e}_{\alpha\beta}$  as a viable alternative to  $\delta_{\alpha\beta}$  as a metric tensor on the globally non-Euclidean, anholonomic space  $\tilde{B}_{int}$ .

Prescription of the plastic strain tensor  $\tilde{C}_{\alpha\beta}^{p} \equiv F_{.\alpha}^{p-1^{A}}G_{AB}F_{.\beta}^{p-1^{B}}$  as a metric  $\tilde{g}_{\alpha\beta}$  was suggested in Eq. (35), following previous work by Miehe [32]. The quantity  $\tilde{C}_{\alpha\beta}^{p}$  is considered to be a well-defined geometric entity with indices referred to the intermediate configuration, since its constituents  $F_{.\alpha}^{p-1^{A}}$  and  $G_{AB}$  are by definition single-valued functions of reference coordinates  $X^{A}$  and time t. This approach appears

especially attractive since for the case of no plastic deformation (and hence no defects or anholonomicity), we have  $F_{\alpha}^{p-1^A} = \delta_{\alpha}^A$  and  $\tilde{g}_{\alpha\beta} = \delta_{\alpha}^A G_{AB} \delta_{\beta}^B$ , thus reducing to the prescription of Simo [31]. However, from the perspective of Eq. (32), this method presents some difficulties, since the plastic strain  $\tilde{C}^{\rm p}_{\alpha\beta}$  would enter the free energy expression  $\tilde{\psi}^{GN}$ , and since we do not view the plastic strain in most cases as a useful state quantity or accurate measure of stored elastic energy. The latter point is of no concern in local theories (e.g. Miehe [32]) wherein higher-order deformation gradients are not explicitly considered and energetic quantities such as  $\tilde{\psi}^{\text{GN}}$  of (32) are not computed. But in nonlocal thermomechanical theories framed in the relaxed intermediate configuration (cf. [27-29]) wherein relations such as (32) are invoked, then we regard the choice of intermediate metric  $\tilde{C}_{\alpha\beta}^{\rm e}$ (34) as more physically plausible than the choice  $\tilde{g}_{\alpha\beta} = \tilde{C}^{\mathrm{p}}_{\alpha\beta}$  (35).

Finally, consider the aforementioned approach of Le and Stumpf [33], with the multiplicative decomposition in component form given by Eq. (37):  $F_A^a = \hat{F}_B^{e^a} \hat{F}_A^{p^B}$ . As discussed already, this decomposition enjoys the simplicity of not requiring any anholonomic basis vectors or corresponding intermediate metric tensor. Moreover, this method offers an alternative viewpoint of kinematics of elastic deformation in terms of the total deformation (between  $B_{ref}$ and  $B_{\rm cur}$ ) of a triad of lattice director vectors assigned to each material point. However, as we have shown in Eq. (50), quantification of the anholonomicity of  $\tilde{B}_{int}$  (i.e., the lack of integrability of  $F_{A}^{p^{\alpha}}$ ) requires knowledge of the anholonomic mapping H, which in turn implies the intermediate configuration metric  $\tilde{g}_{\alpha\beta} = H_{.x}^{-1^{\overline{A}}} G_{AB} H_{.\beta}^{-1^{B}}$  as noted in Eq. (43). (It should be mentioned that the metric  $H_{\alpha}^{-1^A}G_{AB}H_{\beta}^{-1^B}$  is generally non-Euclidean, so this choice does not contradict the non-Euclidean nature of the anholonomic space  $\tilde{B}_{\text{int}}$ .) From the perspective of Eq. (50), since  $H_{B}^{\alpha}$ and its gradient are required, in addition to  $\hat{F}_{A}^{p^{p}}$  and its gradient, this method is more complicated than the other choices (34) and (35), which require only higher gradients of either  $F_{.a}^{p^{\alpha}}$  (Eq. (4)) or  $F_{.a}^{e-1^{\alpha}}$  (Eq. (5)). This aspect leads us to favor  $\tilde{g}_{\alpha\beta} = \tilde{C}_{\alpha\beta}^{e}$  (34) over  $\tilde{g}_{\alpha\beta} = H_{,\alpha}^{-1^A} G_{AB} H_{\beta}^{-1^B}$  (43).

## 6. Concluding remarks

In higher-order gradient plasticity theories couched explicitly upon the mechanics of incompatible defects, special care should be taken when prescribing metric tensors for the anholonomic (e.g., natural or intermediate) configurations that are inherent to the kinematic description, since various scalar products, transpose maps, tensorial symmetry operations, and Jacobian invariants depend explicitly upon the chosen anholonomic basis vectors and their inner product. We discuss several alternative choices to the popular and apparently contradictory (but not incorrect) choice of a Euclidean metric tensor (and accompanying Cartesian basis vectors) attached to an anholonomic (and hence non-Euclidean) configuration space. Endorsed here as an intermediate configuration metric is the pull-back of the current configuration metric tensor by the elastic deformation mapping (i.e., the covariant elastic strain referred to the intermediate configuration).

#### Acknowledgements

J.D.C. and D.L.M. acknowledge the support of the Army Research Office (ARO Award DAAG-559810213). D.J.B. recognizes the support of Sandia National Laboratories. Sandia is a multiprogram laboratory operated by Sandia Corporation, a Lockheed Martin Company, for the United States Department of Energy under Contract DE-AC04-94AL85000.

#### References

- C. Eckart, The thermodynamics of irreversible processes. IV.
   The theory of elasticity and anelasticity, Phys. Rev. 73 (1948) 373.
- [2] K. Kondo, A proposal of a new theory concerning the yielding of materials based on Riemannian geometry, J. Jpn. Soc. Appl. Mech. 2 (1949) 123,146.
- [3] K. Kondo, On the geometrical and physical foundations of the theory of yielding, in: Proceedings of the Second Japan Congress on Applied Mechanics, Japan National Committee for Theoretical and Applied Mechanics, Science Council of Japan, Tokyo, 1953, pp. 41–47.
- [4] B.A. Bilby, R. Bullough, E. Smith, Continuous distributions of dislocations: a new application of the methods of non-Riemannian geometry, Proc. R. Soc. Lond. A 231 (1955) 263.

- [5] E. Kröner, Allgemeine kontinuumstheorie der versetzungen und eigenspannungen, Arch. Rational Mech. Anal. 4 (1960) 273.
- [6] C. Truesdell, W. Noll, The Non-Linear Field Theories of Mechanics, 2nd Edition, Springer, Berlin, 1965.
- [7] C. Teodosiu, Contributions to the continuum theory of dislocations and initial stresses. I, Rev. Roum. Sci. Tech.— Méc. Appl. 12 (1967) 961.
- [8] C. Teodosiu, Contributions to the continuum theory of dislocations and initial stresses. III, Rev. Roum. Sci. Tech.— Méc. Appl. 12 (1967) 1291.
- [9] B.A. Bilby, L.R.T. Gardner, A.N. Stroh, Continuous distributions of dislocations and the theory of plasticity, in: Proceedings of the Ninth International Congress on Applied Mechanics, Vol. 8, Université de Bruxelles, 1957, pp. 35–44.
- [10] E.H. Lee, D.T. Liu, Elastic-plastic theory with application to plane-wave analysis, J. Appl. Phys. 38 (1967) 19.
- [11] W. Noll, Materially uniform simple bodies with inhomogeneities, Arch. Rational Mech. Anal. 27 (1967) 1.
- [12] J.R. Rice, Inelastic constitutive relations for solids: an internal-variable theory and its application to metal plasticity, J. Mech. Phys. Solids 19 (1971) 433.
- [13] J.A. Schouten, Ricci Calculus, 2nd Edition, Springer, Berlin,
- [14] K. Kondo, On the analytical and physical foundations of the theory of dislocations and yielding by the differential geometry of continua, Int. J. Eng. Sci. 2 (1964) 219.
- [15] J.E. Marsden, T.J.R. Hughes, Mathematical Foundations of Elasticity, Dover, New York, 1983.
- [16] K.C. Le, H. Stumpf, Constitutive equations for elastoplastic bodies at finite strain: thermodynamic implementation, Acta Mech. 100 (1993) 155.
- [17] B. Moran, M. Ortiz, C.F. Shih, Formulation of implicit finite element methods for multiplicative finite deformation plasticity, Int. J. Numer. Methods Eng. 29 (1990) 483.
- [18] G.A. Maugin, Eshelby stress in elastoplasticity and ductile fracture, Int. J. Plasticity 10 (1994) 393.
- [19] G.A. Maugin, Material forces: concepts and applications, Appl. Mech. Rev. 48 (1995) 213.
- [20] C. Miehe, E. Stein, W. Wagner, Associative multiplicative elasto-plasticity: formulation and aspects of the numerical implementation including stability analysis, Comput. Struct. 52 (1994) 969.
- [21] K.C. Le, H. Stumpf, Nonlinear continuum theory of dislocations, Int. J. Eng. Sci. 34 (1996) 339.
- [22] C. Teodosiu, A dynamic theory of dislocations and its application to the theory of elastic-plastic continuum, in: Fundamental Aspects of Dislocation Theory, NBS Special Publication 317, US Government Printing Office, Gaithersburg, MD, 1969, pp. 837–876.
- [23] R.W. Lardner, Dislocation dynamics and the theory of the plasticity of single crystals, Z. Angew. Math. Phys. 20 (1969) 514.
- [24] E. Van der Giessen, F.G. Kollmann, On mathematical aspects of dual variables in continuum mechanics. Part 1: mathematical principles, Z. Angew. Math. Mech. 76 (1996) 447.

- [25] H. Stumpf, U. Hoppe, The application of tensor algebra on manifolds to nonlinear continuum mechanics—invited survey article, Z. Angew. Math. Mech. 77 (1997) 327.
- [26] P. Dłużewski, On geometry and continuum thermodynamics of movement of structural defects, Mech. Mater. 22 (1996) 23.
- [27] P. Steinmann, Views on multiplicative elastoplasticity and the continuum theory of dislocations, Int. J. Eng. Sci. 34 (1996) 1717.
- [28] D.J. Bammann, A model of crystal plasticity containing a natural length scale, Mater. Sci. Eng. A 309–310 (2001) 406.
- [29] R.A. Regueiro, D.J. Bammann, E.B. Marin, K. Garikipati, A nonlocal phenomenological anisotropic finite deformation plasticity model accounting for dislocation defects, J. Eng. Mater. Tech. 124 (2002) 380.
- [30] J.C. Simo, M. Ortiz, A unified approach to finite deformation elastoplastic analysis based on the use of hyperelastic constitutive equations, Comput. Methods Appl. Mech. Eng. 49 (1985) 221.

- [31] J.C. Simo, A framework for finite strain elastoplasticity based on maximum plastic dissipation and the multiplicative decomposition: Part I. Continuum formulation, Comput. Methods Appl. Mech. Eng. 66 (1988) 199.
- [32] C. Miehe, A theoretical and computational model for isotropic elastoplastic stress analysis in shells at large strains, Comput. Methods Appl. Mech. Eng. 155 (1998) 193.
- [33] K.C. Le, H. Stumpf, Strain measures, integrability condition and frame indifference in the theory of oriented media, Int. J. Solids Struct. 35 (1998) 783.
- [34] Y.F. Dafalias, Plastic spin: necessity or redundancy?, Int. J. Plasticity 14 (1998) 909.
- [35] S. Takeuchi, A.S. Argon, Steady-state creep of single-phase crystalline matter at high temperature, J. Mater. Sci. 11 (1976) 1542.
- [36] J.C. Gibeling, W.D. Nix, A numerical study of long range internal stresses associated with subgrain boundaries, Acta Metall. 28 (1980) 1743.

## NO. OF

## **COPIES ORGANIZATION**

1 DEFENSE TECHNICAL (PDF INFORMATION CTR ONLY) DTIC OCA

8725 JOHN J KINGMAN RD

STE 0944

FORT BELVOIR VA 22060-6218

1 US ARMY RSRCH DEV &
ENGRG CMD
SYSTEMS OF SYSTEMS
INTEGRATION
AMSRD SS T
6000 6TH ST STE 100
FORT BELVOIR VA 22060-5608

I INST FOR ADVNCD TCHNLGY THE UNIV OF TEXAS AT AUSTIN 3925 W BRAKER LN AUSTIN TX 78759-5316

1 DIRECTOR
US ARMY RESEARCH LAB
IMNE ALC IMS
2800 POWDER MILL RD
ADELPHI MD 20783-1197

3 DIRECTOR
US ARMY RESEARCH LAB
AMSRD ARL CI OK TL
2800 POWDER MILL RD
ADELPHI MD 20783-1197

## ABERDEEN PROVING GROUND

1 DIR USARL AMSRD ARL CI OK TP (BLDG 4600)

# NO. OF COPIES ORGANIZATION

## ABERDEEN PROVING GROUND

30	USA	

AMSRD ARL CI HC

P CHUNG

C CORNWELL

AMSRD ARL WM

M FERMEN COKER

T WRIGHT

J MCCAULEY

AMSRD ARL WM MA

W NOTHWANG

AMSRD ARL WM TA

S SCHOENFELD

AMSRD ARL WM TD

S BILYK

T BJERKE

D CASEM

J CLAYTON (10 CPS)

D DANDEKAR

M GREENFIELD

Y HUANG

K IYER

**B LOVE** 

M RAFTENBERG

E RAPACKI

M SCHEIDLER

S SEGLETES

T WEERASOORIYA

